MH88620BR

## Features

- 900 ohm input impedance
- Externally selectable network balances
- Transformerless 2-4 wire conversion
- Programmable constant resistance feed
- Off-Hook and Dial pulse detection
- High immunity to externally induced longitudinal currents
- Auto ring trip
- On-hook transmission (ANI) capability
- Minimum protection circuitry required
- Compatible with requirements of TELEBRAS DOC/FCC, CSA/UL, CCITT
- Excellent power dissipation (SIL vertical mounting)


## Applications

- On/Off-Premise PBX Line Cards
- Central Office Line Cards

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| :---: | :---: |
| Ordering Information |  |
| MH88620BR $\quad 40$ Pin SIL Package |  |
| $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$ |  |

## Description

The Mitel MH88620BR SLIC provides all of the functions required to interface 2 -wire off premise subscriber loops to a serial TDM, PCM, switching network of a modern PBX. The MH88620BR is manufactured using thick film hybrid technology which offers high voltage capability, reliability and high density resulting in significant printed circuit board area savings. A complete line card can be implemented with very few external components.


Figure 1 - Functional Block Diagram


Figure 2 - Pin Connections

## Pin Description

| Pin \# | Name | Description |
| :---: | :---: | :---: |
| 1 | TIP | Tip Lead. Connects to the TIP lead of the subscriber line. |
| 2 | RING | Ring Lead: Connects to the Ring lead of the subscriber line. |
| 3 | TF1 | Tip Feed 1: Access point for balanced ringing. Normally connects to TF2. |
| 4 | TF2 | Tip Feed 2: Access point for balanced ringing. Normally connects to TF1. |
| 5 | RF1 | Ring Feed 1: Access point for balanced ringing. Normally connects to RF2. |
| 6 | RF2 | Ring Feed 2: Access point for balanced ringing. Normally connects to RF1. |
| 7 | LGND | Battery Ground. $\mathrm{V}_{\text {Bat }}$ return path. Connected to system's energy dumping ground. |
| 8 | LCA | Current Limit Set (Input): The current limit is set by connecting an external resistor as shown in Table 5. For 70 mA default current, this pin is tied to -5 V . |
| 9 | $V_{\text {Bat }}$ | Battery Voltage: Typically -48 V dc is applied to this pin. |
| 10 | NC | No Connection: Reserved. |
| 11 | RGND | Ring Driver Ground Connection. |
| 12 | VRLY | Relay Supply Voltage Connection. |
| 13 | $\overline{\text { RRD }}$ | Ring Relay Drive (Output). Connects to ring relay coil. |
| 14 | RNGC | Ring Relay Control (Input) . |
| 15 | NC | Reserved. No Connection. |
| 16 | TRD | Test Relay Drive (Output): Connects to test relay coil. |
| 17 | TRC | Test Relay Control (Input). |
| 18 | AGND | Analog Ground: $\mathrm{V}_{\mathrm{DD}}$ and $\mathrm{V}_{\mathrm{EE} \text {. }}$ return path. |
| 19 | NC | No Connection: Reserved. |
| 20 | N1 | Network Balance Node 1. An external network balance impedance can be connected between N1 and AGND. See Fig 4. For complex impedances N2 no connection. |
| 21 | N2 | Network Balance Node 2. An external network balance impedance can be connected between N2 and AGND. See Fig 4 N2 connects to GND for $900 \Omega$ balance. |

Pin Description (Continued)

| Pin \# | Name | Description |
| :---: | :---: | :--- |
| 22 | NC | No Connection. Reserved. |
| 23 | Z1 | Line impedance Node 1. Normally connects to Z2. See Fig. 3. |
| 24 | Z2 | Line impedance Node 2. Normally connects to Z1. See Fig 3. |
| 25 | TX | Transmit (Output). 4-wire (AGND) referenced audio output. |
| 26 | RX | Receive (Input). 4-wire (AGND) referenced audio input. |
| 27 | GTX0 | Transmit Gain Node 0. Connects to GTX1 for OdB transmit gain. |
| 28 | GTX1 | Transmit Gain Node 1. Connects to a resistor to AGND for transmit gain adjustment. |
| 29 | GRX0 | Receive Gain Node 0. Connects to GRX1 for OdB gain. |
| 30 | GRX1 | Receive Gain Node 1. Connect to a resistor to AGND for receive gain adjustment. |
| 31 | NC | No Connection. Reserved. |
| 32 | NC | No Connection. Reserved. |
| 33 | NC | No Connection. Reserved. |
| 34 | $\overline{\text { SHK }}$ | Off-Hook Indication (Output). A logic low output indicates when the subscriber <br> equipment has gone Off-Hook. |
| 35.38 | IC | Internal Connection. |
| 39 | VEE | Negative Supply Voltage. -5V dc. |
| 40 | VDD | Positive Supply voltage. +5V dc |

Absolute Maximum Ratings * All voltages are with respect to GNDA unless otherwise stated.

|  | Parameter | Symbol | Min | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Supply Voltages | $\begin{gathered} \hline \text { LGND }-\mathrm{V}_{\text {Bat }} \\ \mathrm{V}_{\mathrm{DD}}-\mathrm{GND} \\ \text { GND }-\mathrm{V}_{\mathrm{EE}} \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline 65 \\ 6 \\ 6 \end{gathered}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| 2 | Storage Temperature | $\mathrm{T}_{\text {S }}$ | -40 | +125 | ${ }^{\circ} \mathrm{C}$ |

* Exceeding these values may cause permanent damage. Functional operation under these conditions is not implied.

Recommended Operating Conditions ${ }^{\dagger}$ - Voltages are with respect to GNDA unless otherwise stated.

|  | Characteristics | Sym | Min | Typ $^{*}$ | Max | Units | Comments |
| :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Operating Temperature | $\mathrm{T}_{\mathrm{OP}}$ | 0 |  | 70 | ${ }^{\circ} \mathrm{C}$ |  |
| 2 | Supply Voltages | $\mathrm{V}_{\mathrm{Bat}}$ | -44 | -48 | 70 | V |  |
|  |  | $\mathrm{~V}_{\mathrm{DD}}$ | 4.75 | +5.0 | -60 | V |  |
|  |  | $\mathrm{~V}_{\mathrm{EE}}$ | -4.75 | -5.0 | 5.25 | V |  |
|  |  |  |  | 5 | -5.25 | V |  |
|  |  |  |  |  |  |  |  |

* Typical figures are at $25^{\circ} \mathrm{C}$ and are for design aid only; not guaranteed and not subject to production testing. $\dagger$ Voltages specified are with respect to LGND.


## DC Electrical Characteristics*

|  |  | Characteristics | Sym | Min | Typ ${ }^{\ddagger}$ | Max | Units | Test Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 |  | Operating Loop Current <br> Variation in Loop Current from nominal | Loop <br> $\mathrm{I}_{\text {Loop }}$ | $\begin{aligned} & 17 \\ & 16 \end{aligned}$ | $\pm 2$ | 70 | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \\ & \mathrm{~mA} \end{aligned}$ | $\begin{aligned} & \mathrm{R}_{\text {Loop }}=0 \Omega, \mathrm{LCA}=-5 \mathrm{~V} \\ & 1500 \Omega \\ & 2000 \Omega \mathrm{~V}_{\text {Bat }}=-48 \mathrm{~V} \end{aligned}$ |
| 2 |  | Operating Current <br> Power Dissipation | $\begin{gathered} \mathrm{I}_{\mathrm{Bat}} \\ \mathrm{I}_{\mathrm{DD}} \\ \mathrm{I}_{\mathrm{EE}} \\ \text { PDo } \\ \text { PD1 } \end{gathered}$ |  | $\begin{gathered} 2 \\ 15 \\ 15 \\ \\ 2 \\ 250 \end{gathered}$ |  | $\begin{gathered} \mathrm{mA} \\ \mathrm{~mA} \\ \mathrm{~mA} \\ \mathrm{~W} \\ \mathrm{~mW} \end{gathered}$ | $\mathrm{R}_{\text {Loop }}=$ Open (On-hook) On-Hook or Off-Hook On-Hook or Off-Hook <br> Active <br> Stand-by/Idle |
| 3 | $\overline{\text { SHK }}$ | Low Level Input Voltage High Level Input Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{OL}} \\ & \mathrm{~V}_{\mathrm{OH}} \end{aligned}$ | 3.7 |  | 0.5 | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{I}_{\mathrm{OL}}=400 \mu \mathrm{~A} \\ & \mathrm{I}_{\mathrm{OH}}=40 \mu \mathrm{~A} \end{aligned}$ |
| 4 | $\frac{\overline{\mathrm{RNGC}}}{\overline{\mathrm{TRC}}}$ | Low Level Input Voltage High Level Input Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{IL}} \\ & \mathrm{~V}_{\mathrm{IH}} \end{aligned}$ | 2.4 |  | 0.8 | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |  |
| 5 |  | Low Level Input Current High Level Input Current | $\begin{aligned} & I_{\mathrm{IL}} \\ & I_{\mathrm{IH}} \end{aligned}$ |  |  | $\begin{aligned} & 20 \\ & 20 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mu \mathrm{A} \\ & \mu \mathrm{~A} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{IL}}=0.0 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{IH}}=5.0 \mathrm{~V} \end{aligned}$ |

* DC Electrical Characteristics are over recommended operating conditions unless otherwise stated.
$\ddagger$ Typical figures are at $25^{\circ} \mathrm{C}$ with nominal $\pm 5 \mathrm{~V}$ supplies and are for design aid only.

AC Electrical Characteristics*

|  | Characteristics | Sym | Min | Typ ${ }^{\ddagger}$ | Max | Units | Test Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Analog Tx Gain (T-R to TX) |  |  | 0 |  | dB | Externally adjustable |
| 2 | Analog Rx Gain (RX to T-R) |  |  | 0 |  | dB | Externally adjustable |
| 3 | Ringing Capability |  | 25 |  |  | $\mathrm{V}_{\text {RMS }}$ | $\begin{aligned} & \mathrm{R}_{\text {Loop }}=1400 \Omega \\ & \text { Term. } 6.8 \mu \mathrm{~F}+200 \Omega \end{aligned}$ |
| 4 | On-hook Transmission Signal input level Gain |  | 4 |  | $\begin{gathered} 2.0 \\ 8 \end{gathered}$ | $\mathrm{V}_{\text {RMS }}$ dB | $\begin{aligned} & \mathrm{V}_{\text {Bat }}=-48 \mathrm{~V} \\ & \mathrm{~T}-\mathrm{R} \text { load }=10 \Omega \mathrm{k} \text { min. } \end{aligned}$ |
| 5 | SHK Rise Time Fall time | $\begin{aligned} & t_{R} \\ & t_{F} \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ |  | msec <br> msec | Dial Pulse Detection |
| 6 | 2 Wire Termination Impedance |  |  | 900 |  | $\Omega$ | Adjustable |
| 7 | Off-Hook Detect Threshold |  |  | 10 |  | mA |  |
| 8 | $\begin{aligned} & \text { 2-Wire Return Loss } \\ & 900 \Omega \text { at T-R } \\ & \mathrm{Zin}=900 \Omega \\ & 900 \Omega+2.16 \mu \mathrm{~F} \text { at T-R } \\ & \mathrm{Zin}=900 \Omega \end{aligned}$ |  | $\begin{aligned} & 20 \\ & 26 \\ & 20 \\ & 14 \\ & 18 \\ & 14 \end{aligned}$ |  |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB | $\begin{aligned} & 300-500 \mathrm{~Hz} \\ & 500-2500 \mathrm{~Hz} \\ & 2500-3400 \mathrm{~Hz} \\ & 300 \mathrm{~Hz} \\ & 600-2000 \mathrm{~Hz} \\ & 3400 \mathrm{~Hz} \end{aligned}$ |
| 9 | Longitudinal Balance <br> Longitudinal to Metallic |  | $\begin{aligned} & 58 \\ & 55 \\ & 53 \end{aligned}$ |  |  | dB <br> dB <br> dB | $\begin{aligned} & 2000 \mathrm{~Hz}, 1000 \mathrm{~Hz} \\ & 2000 \mathrm{~Hz}, 3000 \mathrm{~Hz} \\ & 3400 \mathrm{~Hz} \end{aligned}$ |
| 10 | Longitudinal Current Capability |  |  |  | 40 | mA | 20mA per lead |
| 11 | Idle Channel Noise Rx to T-R T-R to Tx | $\mathrm{N}_{\mathrm{CR}}$ $\mathrm{N}_{\mathrm{CX}}$ |  | $\begin{gathered} 8 \\ 12 \end{gathered}$ |  | dBrnc dBrnc |  |
| 12 | Transhybrid Loss <br> Tx gain 0dB Rx gain 0dB | THL | $\begin{aligned} & 16 \\ & 20 \\ & 16 \\ & \hline \end{aligned}$ |  |  | dB <br> dB <br> dB | $\begin{aligned} & 300-500 \mathrm{~Hz} \\ & 500-2500 \mathrm{~Hz} \\ & 2500-3400 \mathrm{~Hz} \\ & \hline \end{aligned}$ |
| 13 |  |  |  |  |  |  |  |
| 14 | Analog Signal Overload Level at TIP and RING |  |  |  | 4 | dBm | $\begin{aligned} & \hline \mathrm{T}-\mathrm{R}=900 \Omega \\ & \mathrm{~V}_{\text {Bat }}=-48 \mathrm{~V} \end{aligned}$ |
| 15 | Ringing Signal Voltage |  | 70 | 80 | 90 | $\mathrm{V}_{\text {RMS }}$ |  |
| 16 | Ringing Frequency |  | 20 | 25 | 30 | Hz |  |
| 17 | Ring Trip Delay |  |  | 100 |  | ms |  |
| 18 | Absolute Gain variation |  | -25 | 0 | +. 25 | dB | 0dBm at T-R, 1 kHz |
| 19 | Relative Gain, reference to 1kHz |  | -2 | 0 | +. 2 | dB | $300-3400 \mathrm{~Hz}$ |
| 20 | Power Supply Rejection Ratio $\begin{aligned} & \mathrm{V}_{\mathrm{Bat}} \\ & \mathrm{~V}_{\mathrm{DD}} \\ & \mathrm{~V}_{\mathrm{EE}} \end{aligned}$ | PSRR | $\begin{aligned} & 24 \\ & 24 \\ & 24 \\ & \hline \end{aligned}$ | $\begin{aligned} & 30 \\ & 30 \\ & 30 \\ & \hline \end{aligned}$ |  | dB | 1 kHz , 100mVpp |

* AC Electrical Characteristics are over Recommended Operating Conditions unless otherwise stated.
$\ddagger$ Typical figures are at $25^{\circ} \mathrm{C}$ with nominal $\pm 5 \mathrm{~V}$ supplies and are for design aid only.
Note: Test Conditions use a transmit and receive gain set to 0 dB default and a $\mathrm{Z}_{\text {in }}$ value of $900 \Omega$ unless otherwise stated.
"Ref" indicates reference impedance which is equivalent to the termination impedance.
"Net" indicates network balance impedance.

| Transmit Gain (dB) <br> 2-Wire to Tx 20log <br> (Tx/2-Wire) | RTX Resistor (1\%) <br> Value ( $\Omega$ ) | Notes |
| :---: | :---: | :--- |
| +6.0 | No Resistor |  |
| +4.0 | 38.3 k | Results in OdB overall gain when used with <br> Mitel A-law codec (i.e. MT8965) |
| +3.7 | 32.4 k |  |
| 0.0 | Connect GTX0 to GTX1 |  |
| -3.0 | 5.49 k |  |
| -6.0 | 3.32 k |  |
| -12.0 | 1.43 k |  |

Note 1. Overall gain refers to the receive path of PCM to 2-Wire.
Note 2 See Figure 2 for Application Circuit.

| Receive Gain (dB) <br> Rx to 2-Wire 20log <br> (2-Wire/ Rx) | RRX Resistor (1\%) <br> Value ( $\Omega$ ) | Notes |
| :---: | :---: | :--- |
| +6.0 | No Resistor |  |
| 0.0 | 5.49 k |  |
| +3.0 | 4.87 k |  |
| -3.7 | 4.64 k | Results in 0dB overall gain when used with <br> Mitel A-law codec (i.e. MT8965) |
| -4.0 |  |  |
| -6.0 | 3.32 k |  |
| -12.0 | 1.43 k |  |

Note 1. Overall gain refers to the receive path of PCM to 2-Wire. Note 2. See Figure 2 for Application Circuit.


## Functional Description

The SLIC uses a transformerless electronic 2-4 wire converter which can be connected to a Codec to interface the 2 wire subscriber loops to a time division multiplexed (TDM) pulse code modulated (PCM) digital switching network. For analog applications, the TXRX of the 2 wire converter can be connected directly to an analog crosspoint switch, such as the MT8816. Powering of the line is provided through precision battery feed resistors. The MH88620BR also contains control, signalling and status circuitry solution which combines to provide a complete functional solution, simplifying the manufacture of line cards. This circuitry is illustrated in the functional block diagram in Fig 1. The MH88620BR is designed to be pin compatible with Mitel's MH88632, MH88625 and MH88628. This allows a common PCB design with common gain, input impedance and network balance.

## Approvals

FCC part 68, CCITT, DOS CS-03, UL 1459, CAN/ CSA-22.2 NO. 225-M90 and ANSI/EIA/TIA-464-A are system level safety standards and performance requirements. As a component of a system, the MH88620BR is designed to comply with the applicable requirements of these specifications.

## Battery Feed

The loop current for the subscriber equipment is sourced through a pair of matched 200 ohm resistors connected to the TIP and RING. The two wire loop is biased such that the Ring lead is 2 V above VBAT (typically -46V) and the TIP lead is 2 V below LGND (typically -2 V ) during constant voltage mode.

The SLIC is designed for a nominal battery voltage of -48 Vdc and can provide the maximum loop current of 70 mA under this condition.

The interface circuit is designed to be operated down to a maximum of 16 mA dc , with a battery voltage of -44 . The Tip and Ring output drivers can operate within 2 V of VBAT and LGND rails.

## Loop Current Setting

The MH88620BR SLIC is a constant resistance with constant voltage fallback design. This design feature provides for long loop capability regardless of the current setting. Refer to graph 1.

The LCA (Loop Current Adjust) pin is an input to an internal resistor driver network which generates a bias voltage. The loop current is proportional to this voltage. The loop current can be set between 20 and 70 mA by various connections to the LCA pin as illustrated in Table 5 and Figure 5. The loop current during a fault condition will be limited to the constant loop current programmed. Primary over current protection is inherent in the current limiting feature of the 200 ohm battery feed resistor. Refer to Graph 1.

## Receive and Transmit Audio Path

The audio signal of the 2 -wire is sensed differentially across the 200 ohm feed resistor and is passed on to a second differential amplifier stage in the $2 \mathrm{~W} / 4 \mathrm{~W}$ conversion block. This block sets the transmit gain on the 4 -wire side and cancels signals originating from the receive input.

## Programmable Transmit and Receive Gain

Transmit Gain (Tip-Ring to Tx) and Receive Gain (Rx to Tip-Ring) are programmed by connecting external resistors (RRX and RTX) from GRX1 to AGND and from GTX1 to AGND as indicated in Figure 2 and Table 1 and 2. The programmable gain range is from -12 dB to +6 dB ; this wide range will accommodate any loss plan. Alternatively, the default Receive Gain of 0 dB and Transmit Gain of 0 dB can be obtained by connecting GRX0 to GRX1 and GTX0 to GTX1. In addition, a Receive Gain of +6 dB and Transmit Gain of +6 dB can be obtained by not connecting resistors RRX and RTX. For correct gain programming. the MH88620BR's Tip-Ring impedance (Zin) must match the line termination impedance.

For optimum performance, resistors RRX should be physically located as close as possible to the GRX1 input pin, and resistor RTX should be physically located as close as possible to the GTX1 input pin.

## Two Wire Port Termination Impedance

The AC termination of 900 ohms, of the 2 W port is set using active feedback paths to give the desired relationship between the line voltage and the line current. The loop current is sensed differentially across the two feed resistors and converted to a single ended signal. This signal is fed back to the Tip/Ring driver circuitry such that impedance in the feedback path gets reflected to the two wire port.

The MH88620BR's Tip-ring impedance (Zin) is designed to be $900 \Omega$, when used with $25 \Omega$ PTC's as protection circuitry. For this requirement, Z1 and Z2 should be connected together on the PCB. To accommodate the use of lower value PTC's a series
resistance can be connected between Z 1 and Z 2 . For example, it two $8 \Omega$ PTCs are used, connect $340 \Omega$ between Z1 and Z2. The design uses a 0.1 times impedance amplifier so the $340 \Omega$ actually adds $34 \Omega$ of additional impedance to the $850 \Omega(16+34+$ $850=900$ ). For complex impedance setting, a capacitor and/or resistor can be connected between Z1 and Z2. For example, if Return Loss is to be maximised for a Zin of $900+2.2 \mu \mathrm{~F}$, a $0.22 \mu \mathrm{~F}$ cap can be connected between Z 1 and Z 2 .

## Network Balance

Transhybrid loss is maximised when the line termination impedance and SLIC network balance are matched. The MH88620BR's network balance impedance can be set to Zin, or to a user selectable value. Thus, the network balance impedance can be set to any Brazilian or other international requirement. An external Network Balance impedance is selected which 0.1 times the impedance between N1 and AGND. N2 to GND balances to $900 \Omega$.

## Off-Hook and Dial Pulse Detection

The $\overline{\text { SHK }}$ pin goes low when the DC-loop current exceeds a specified level. The threshold level is internally set by the bias voltage of the switch-hook detect circuitry.

Dial pulses can be detected by monitoring the interruption rate at the SHK pin. These dial pulses would be debounced by the system software.

## Ring Trip Detection

The interface permits detection of an Off-Hook condition during ringing. If the subscriber set goes Off-Hook when the ringing signal has been applied, the DC loop current flow will be detected within approximately 100 msecs and the SHK output will go low. The ring relay is automatically disabled by the internal hardware.

## Longitudinal Balance

The longitudinal balance specifies the degree of common mode rejection in the 2 to 4 wire direction. Precision laser trimming of internal resistors in the hybrid ensures good overall longitudinal balance.

The interface circuitry can operate in the presence of induced longitudinal currents of up to 40 mA RMS at 60 Hz .

## DTMF

The DTMF tones are transmitted and received at the 4 -wire port.

## High voltage Capability

Inherent in the thick-film process is the ability of the substrate to handle high voltage. The standard Mitel thick-film process provides dielectric strengths of greater than 1000 VAC or 1500 VDC. The thick-film process allows easy integration of surface mount components such as the high voltage bipolar power transistor line drivers. This allows for simpler, less elaborate and less expensive protection circuitry required to handle high voltage transcients and fault conditions caused by lightning, induced voltages and power line crossings.

## On-Hook Transmission

The MH88620BR provides for on-hook transmission which supports features such as Automatic number identification (ANI). The ANI information is a FSK or DTMF signal originating from and sent by the C.O. during the off period of the ringing voltage being sent to the subscriber's set. The signal is present during the off period between the first and second ring. The subscriber's set decodes the identification signal and displays the calling party's number.

## Loop Length

The MH88620BR can accommodate loop lengths of up to 2000 ohms minimum (including the subscriber equipment). This corresponds to approximately 8kmusing \#26 AWG twisted pair or 15 km using \#24 AWG twisted pair.

## Applications

As shown in the application diagram, Figure 7, the ringing voltage, typically $80 \mathrm{~V}_{\text {RMS }} 25 \mathrm{~Hz}$ biased at -VBAT, is applied to the subscriber line through an external relay, K1, K1 is a DPST 2-form-C, EM (electro-mechanical) relay which switches protection diodes D3 and D4 out when Ringing is switched in, K1 is enabled by applying a logic low level to the relay driver control input, RNGC.

An additional relay driver is provided to control an $\mathrm{In} /$ Out Test Bus relay, K2. K2 is a DPST 2 -form-C, EM relay which is enabled by applying a logic low level to the relay driver control input.

## Protection Circuitry

Primary protection, from lightning strikes and AC line faults, is normally located in the MDF (main distribution feeder) which is located external to the PABX or CO switching system. The primary protection circuitry is normally housed in a 5 -pin connector and consists of either carbon blocks, with spark gaps (older technology), gas discharge limits the high voltage to approximately 300 to 500 volts before entering the switching system. Secondary protection, in the switching system, is required to further limit these high voltages/ currents. Secondary protection is normally implemented on each line card and is designed to protect the SLICs from permanent damage. The basic secondary high voltage
protection circuitry for the MH88620BR, as illustrated in Figure 7, consists of PTC1, PTC2 and clamping diodes D1 to D4. During a fault condition, the diodes clamp the overvolt Ground and -VBAT. PTC1 and PTC2 current limit as their resistance increases with power dissipation caused by the over-voltage/ over-current condition. The ground that D1 and D3 are connected to, must be an EDG (energy dumping ground) which is connected to the chassis or system ground. This is a seperate conductor from LPGND or AGND on the line card PCB. D2 and D4 conduct the energy into a -VBAT supply which is a seperate conductor from the -VBAT feed supply to the SLICs. A power MOSFET circuit as shown in Figure 8, can be used to divert the energy normally dumped into -VBAT, the EDG conductor. Usually one MOSFET circuit can be used for 16 SLICs or per line card.

Depending on the additional level of protection required, PRO1 and/or PRO2 protectors may be used. These are used to protect the SLICs Ring sense resistor and/or Ring generator, from being damaged if a fault condition occurs during the application of Ringing to the line. PRO2 can be implemented using two back to back zener diodes, or an equivalent transcient suppressor.

The clamping voltage should be $>16 \mathrm{Vdc}$ and $<26 \mathrm{Vdc}$. PRO2 may not be required depending on the value and power dissipation of PRO1.


Notes
a) to accommodate the use of $2 \times 25 \Omega$ PTCs, connect $Z 1$ and $Z 2$ together, $Z_{i n}=900 \Omega$.
b) to accommodate the use of $2 \times 8 \Omega$ PTCs, connect $340 \Omega$ between $Z 1$ and $Z 2=900 \Omega$.
c) to accommodate the use of $2 \times 25 \Omega$ PTCs, connect $0.22 \mu \mathrm{~F}$ between Z 1 and $Z 2=900 \Omega+2.2 \mu \mathrm{~F}$.

| Loop Current | LCA Pin Connection | Reference Fig \# |
| :---: | :--- | :---: |
| 20 | Connect $10 \mathrm{k} \Omega$ from LCA to +5 V. | 5 a |
| 25 | Connect $16 \mathrm{k} \Omega$ from LCA to +5 V. | 5 a |
| 30 | Connect $36 \mathrm{k} \Omega$ from LCA to +5 V. | 5 a |
| 35 | Leave LCA open circuit | 5 c |
| 40 | Connect $24 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 45 | Connect $10 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 50 | Connect $5.6 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 55 | Connect $2.4 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 60 | Connect $1.3 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 65 | Connect $680 \mathrm{k} \Omega$ from LCA to -5 V | 5 b |
| 70 | Connect LCA to -5 V | 5 d |

Table 5 - Loop Current Setting

$\mathrm{Z}_{\text {in }}=0.1 \times\left[\mathrm{RS}+\frac{1}{1 / R P+(S \times C P)}\right]$
where $S=j \times w$
and $w=2 \times J C \times f$
Notes:

1) The $10 x$ Zin network must be set to $10 x$ the desired input Zin (impedance).
2) The $10 \times$ NETBAL network must be set to10x the desired network balance.

## Example:

3) Make connection between N1 and component as short as possible.

If $\mathrm{RS}=0 \Omega, \mathrm{RP}=800 \Omega, \mathrm{CP}=.5 \mathrm{nf}$ Then the network balance is $800 \Omega$ in parallel with 50 nF .

Figure 4 - External Network Balance Setting


Figure 5 - Loop Current Setting


Figure 6 - Gain Programming with External Components


Figure 7a - OPS SLIC Configuration Applications Circuit


Figure 7b - OPS SLIC Configuration Applications Circuit - Balanced Ringing


Figure 7c-16 Lines Circuit Configuration

Side View

$4.20 \pm 0.020$
$(50.8 \pm 0.5)$

